

Numerical simulation techniques for the efficient and accurate treatment of local fluidic transport processes together with chemical reactions

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Scientific goals

Extend the up-to-now developed and validated methodology and realize the corresponding software implementation in the CFD package FEATFLOW.

The main numerical ingredients to be combined/extended are the following:

- high-resolution <u>Algebraic Flux Correction (AFC)</u> stabilization schemes to suppress numerical diffusion and to prevent nonphysical oscillations
- locally adaptive <u>Grid Deformation (GD)</u> techniques applied on (general) unstructured meshes with the aim to obtain high-resolution computational meshes satisfying additional requirements on the relative orientation with respect to local velocity fields in order to further decrease the extent of numerical diffusion
- time-scale independent reaction modules for the treatment of mutually coupled <u>fast chemical reactions</u> supplemented with appropriate models to reflect the extent of segregation of the individual species



High-resolution AFC stabilization

$$\frac{\partial c}{\partial t} + \nabla \cdot (\mathbf{v}c) - \alpha \Delta c = f(c) \qquad \text{with} \quad \alpha \to 0$$

Standard discretizations face shortcomings for nonsmooth solutions

- Low order methods lead to smearing
- High order methods introduce unphysical oscillations (potentially leading to simulation blowup)

Remedy: Algebraic Flux Correction method

- Local extremum diminishing (+)
- Positivity preserving (+)
- Transforms the linear problem to a non-linear one (-)
- Robust and highly accurate (+)



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PDE-free mesh deformation method

- Construction of (dynamic) monitor function (distance to interface, curvature, concentration gradients, vorticity
- Anisotropic Laplace smoothening (fast)
- Arbitrary Lagrangian-Eulerian Method (ALE) for non-stationary problems
- Handling geometrically complex/dynamic problems in the framework of FBM



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Ses Reaktive Blasenströmungen

Simulation of chemical reactions (preliminary work within the SPP 1740)

 $A + B \xrightarrow{k \to \infty} P \qquad \partial_t \phi + u \cdot \nabla \phi = \nabla \cdot (d\nabla \phi) \text{ with } \phi = c_A - c_B \text{ Toor and Chiang}$ Adopted simulation technique: Simultaneous use of two meshes /discretizations: - equidistant, structured, low resolution for velocity - deformed, structured, high resolution for passive/active scalar Efficient and robust interpolation from mesh to mesh in parallel framework Transported scalar field ϕ Monitor function Computational mesh figure q = 0 Monitor function Computational



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Simulation of the super-focus mixer (SFM)



Geometry of the final SFM with visualization of the reactants

Intermediate SFM geometry and operation conditions

Mixing chamber: length: 22.5 mm initial width: 19.9 mm height: 500 µm opening angle: 50°



Intantaneous reaction scheme: $A + B \xrightarrow{k \to \infty} P$

Investigated flowrates: 100 mL/h 250 mL/h 500 mL/h

$$D_{A,B} = 3.0 \cdot 10^{-10} \ m/s^2$$

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Computationally obtained flowfield in the Superfocus mixer

Flowrate: $\dot{V} = 100 \ mL/h$

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Computationally obtained flowfield in the Superfocus mixer

Flowrate: $\dot{V} = 250 \ mL/h$

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Computationally obtained flowfield in the Superfocus mixer

Flowrate: $\dot{V} = 500 \ mL/h$

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Exploiting the two-fold symmetry only the $\frac{1}{4}$ of the domain needs to be meshed. NEL($\frac{1}{4}$) = 1.2·10⁶ elements. Velocity is interpolated in an L_2 sense to the deformed mesh.

Reaktive

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