

Simulation of rising bubbles using a new multiple relaxation time lattice Boltzmann method coupled with level set interface capturing

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The Lattice Boltzmann Method technische universität dortmund

General LBE with single relaxation collision based on Maxwell equilibrium

$$\frac{\partial f_k}{\partial t} + e_k \cdot \nabla f_k = \frac{1}{\tau} (f_k - f_k^{eq}) + \frac{(e_k - u_i) \cdot F_i}{\rho c_s^2} f_k^{eq}$$

Recovers the nearly incompressible N.E. equations through the Chapman-Enskog expansion

$$\partial_t(\rho u_j) + \partial_i(\underbrace{\frac{1}{3}\rho\delta_{ij}}_{\rho} + \rho u_i u_j) - \underbrace{\frac{1}{3}\left(\tau - \frac{1}{2}\right)}_{\nu}\partial_i\left[\partial_j(\rho u_i) + \partial_i(\rho u_j)\right] = F_j$$

Pressure is simply recovered by an equation of state (EOS)

ideal gas EOS
$$P = \frac{1}{3}\rho$$



► Continuum Surface Force (CSF) form of LBM

• Turn the N.E. into a desired form for LBM (Mehravaran, 2011)

$$\partial_t \mathbf{u} + \mathbf{u} \cdot \nabla \mathbf{u} + \frac{\nabla P}{\rho(\phi)} - \frac{\nabla \cdot \left(\mu(\phi)(\nabla \mathbf{u} + \nabla \mathbf{u}^T)\right)}{\rho(\phi)} = -\frac{\sigma \kappa(\phi) \mathbf{n}(\phi) \delta_{\varepsilon}(\phi)}{\rho(\phi)}$$

• Assume virtual variables $\bar{\rho} = 1$ and $\bar{\mu} = \mu/\rho$ and move the $\frac{\nabla P}{\rho(\phi)}$ to the rhs

$$\bar{\rho}(\phi)\partial_t u + \bar{\rho}(\phi)\mathbf{u} \cdot \nabla \mathbf{u} + \nabla P - \bar{\mu}(\phi)\nabla \cdot (\nabla \mathbf{u} + \nabla \mathbf{u}^{\mathsf{T}}) = \bar{F}$$

• The new rhs force takes the form

$$\bar{\pmb{\mathsf{F}}} = -\frac{\sigma\kappa(\phi) \pmb{\mathsf{n}}(\phi) \delta_{\varepsilon}(\phi)}{\rho(\phi)} + \frac{\nabla \mu(\phi) \cdot (\nabla \pmb{\mathsf{u}} + \nabla \pmb{\mathsf{u}}^{\mathsf{T}})}{\rho(\phi)} + \nabla P\left(1 - \frac{1}{\rho(\phi)}\right)$$



► Time Integration

• Forward Euler for the collision term, Crank-Nicolson for the forces

$$f_{k}(x+e_{k}\Delta t,t+\Delta t) = f_{k}(x,t) - \sum_{j} \Lambda_{k,j}(f_{j}(x,t)-f_{j}^{eq}(x,t)) + \frac{\Delta t}{2}S_{k}\Big|_{(x,t)} + \frac{\Delta t}{2}S_{k}\Big|_{(x+e_{k}\Delta t,t+\Delta t)}$$

where $S_{k} = \frac{(e_{k,i}-u_{i})\cdot\bar{F}_{i}}{\rho c_{s}^{2}}f_{k}^{eq}$

• Recast into an explicit form for $g_k = f_k - \frac{\Delta t}{2}S_k$

$$g_k(x+e_k\Delta t, t+\Delta t) = g_k(x,t) - \sum_j \Lambda_{k,j}(g_j(x,t)-g_j^{eq}(x,t)) + (I-\frac{1}{2}\Lambda_{k,j})S_j(x,t)$$

Velocity
$$\bar{\rho}u_i = \sum_k e_{k,i}g_k + 0.5\bar{F}_i$$
, Pressure $P = \frac{\bar{\rho}}{3} = \frac{1}{3}\sum_k g_k$



► Force Discretization; Central differencing approach

- discretization along major directions; (X, Y)
- central differences for $\nabla \mathbf{u}, \nabla \phi, \nabla P$ (∇a in general)

$$\frac{\partial a(x,y)}{\partial x} = \frac{a(x+h,y) - a(x-h,y)}{2h}$$
$$\frac{\partial a(x,y)}{\partial y} = \frac{a(x,y+h) - a(x,y-h)}{2h}$$

• perform the dot product of the force terms as in

$$S_k = \frac{(e_{k,i} - u_i) \cdot \bar{F}_i}{\rho c_s^2} f_k^{eq}$$



► Force Discretization; Directional approach

- discretizing the $(e_k \cdot \nabla)$ terms along the lattice directions, e_k
- central differences for $(e_k \cdot \nabla \mathbf{u})$ and $(e_k \cdot \nabla \phi)$
- *P* ≈ *O*(*f_k*), so we perform an averaged differencing for (*e_k* · ∇*P*) (Lee, Lin, 2005)

$$(e_k \cdot \nabla P)^C = \frac{P(x+e_k\Delta t) - P(x-e_k\Delta t)}{2}$$

$$(e_k \cdot \nabla P)^B = \frac{-P(x+2e_k\Delta t)+4P(x+e_k\Delta t)-3P(x))}{2}$$

Averaged difference $(e_k \cdot \nabla P)^{Avg} = \frac{(e_{k,i} \cdot \partial_i P)^C + (e_{k,i} \cdot \partial_i P)^B}{2}$



► Solving the Level Set equation

 $\partial_t \phi + \mathbf{u} \cdot \nabla \phi = 0$ where $\phi(\mathbf{x}) = 0$ at $X = \Gamma$

- 2nd order Runge-Kutta time integration
- 5th order WENO finite difference for the convective term
- weighted reinitialization to the approximated signed distance function every $\triangle T$

$$\phi_{\textit{new}} = \alpha \phi_{\textit{dist}} + (1 - \alpha) \phi_{\textit{old}}$$

• regularized *Heaviside* function $H(\phi)$, for density and viscosity profiles

$$\begin{cases} \rho(\phi) = \rho_I H(\phi) + \rho_g (1 - H(\phi)) \\ \mu(\phi) = \mu_I H(\phi) + \mu_g (1 - H(\phi)) \end{cases}$$

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► Static bubble; Case 1

Density ratio : $\rho_l/\rho_g = 10$ Viscosity ratio: $\mu_l/\mu_g = 10$

Spurious velocity level





► Static bubble; Case 1

Pressure and velocity errors

Shan-Chen LB Model						
1/ <i>h</i> 40 80 160 320						
U _{max}	6.5e-5	1.4e-4	3.00e-4	6.24e-4		
$\left \bigtriangleup P - \sigma / r_0 \right / (\sigma / r_0)$	0.0453	0.0172	0.0017	0.0023		

LBM-Level Set, Approach 1						
1/ <i>h</i> 40 80 160 320						
U _{max}	5.8e-5	3.00e-5	9.8e-6	7.4e-6		
$\left \bigtriangleup P - \sigma / r_0 \right / (\sigma / r_0)$	0.0108	0.0126	0.0087	0.0058		

LBM-Level Set, Approach 2					
1/h	40	80	160	320	
U _{max}	1.93e-5	8.2e-6	4.6e-6	2.6e-6	
$\Delta P - \sigma/r_0 / (\sigma/r_0)$	0.0277	0.0147	0.0086	0.0060	

Numerical Results



► Static bubble; Case 2

Density ratio : $\frac{\rho_I}{\rho_g} = 1000$ Viscosity ratio : $\frac{\mu_I}{\mu_g} = 100$





► Static bubble; Test Case 2

Pressure and velocity errors

LBM-Level Set, Approach 1

1/h	40	80	160	320
U _{max}	4.7e-6	5.0e-6	3.0e-6	2.1e-6
$\left \bigtriangleup P - \sigma / r_0 \right / (\sigma / r_0)$	0.7520	0.4250	0.1331	0.0249

LBM-Level Set, Approach 2

1/h	40	80	160	320
U _{max}	5.7e-6	4.1e-6	8.4e-7	3.6e-7
$\left \bigtriangleup P - \sigma / r_0 \right / (\sigma / r_0)$	0.1611	0.0211	0.0080	0.0060

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► Rising bubble; Test Case 1

"Proposal for quantitative benchmark computations of bubble dynamics" (2007) Hysing, S.; Turek, S.; Kuzmin, D.; Parolini, N.; Burman, E.; Ganesan, S.; Tobiska, L.



see www.featflow.de/benchmarks/

$ ho_{\rm I}/ ho_{\rm g}$	$\mu_{\rm I}/\mu_{\rm g}$	Eo	Re
10	10	10	35

$$Eo = rac{4
ho_{l}gr_{0}^{2}}{\sigma}$$
 , $Re = rac{
ho_{l}\sqrt{g}(2r_{0})^{3/2}}{\mu_{l}}$



► Rising bubble; Test Case 1

Bubble at T = 3, Grid: 160×320





► Rising bubble; Test Case 1

Benchmarking time evolution, 0 < T < 3





▶ Rising bubble; Test Case 1 \Rightarrow LBM-LS Approach 2, grid effect, 0 < T < 3





▶ Rising bubble; Test Case 1 \Rightarrow Benchmark comparison, 320×640 , 0 < T < 3





► Rising bubble; Test Case 1

Error Reduction Rate

1/h	e ₁	ROC1	e ₂	ROC ₂	$\parallel e_{\infty} \parallel$	ROC_∞
			Rise Velocity			
40	0.076750		0.149206		0.177204	
80	0.028549	1.426712	0.053590	1.477261	0.055123	1.684686
160	0.007367	1.954169	0.013609	1.977321	0.024643	1.161464

LBM-Level Set, Approach 1

LBM-Level Set, Approach 2

1/h	e ₁	ROC1	e ₂	ROC ₂	$\parallel e_{\infty} \parallel$	${ m ROC}_\infty$
			Rise Velocity			
40	0.096958		0.051369		0.046389	
80	0.042549	1.188226	0.021663	1.245647	0.020337	1.189679
160	0.013890	1.615036	0.000692	1.644344	0.000757	1.424072



► Rising bubble; Test Case 2





• Rising bubble; Test Case 2 LBM-LS Approach 2, 160×160 , 0 < T < 3





► Rising bubble; Test Case 2

Bubble at T = 3, Grid: 160×320





▶ Rising bubble; Test Case 2 \Rightarrow LBM-LS Approach 2, grid effect, 0 < T < 3





► Rising bubble; Test Case 2 ⇒ Benchmarking the picture norm!





▶ Rising bubble; Test Case 2 \Rightarrow Benchmark comparison, 320×640 , 0 < T < 3



Numerical Results



► Computational Performance



- OpenMP implementation on Intel Xeon 1.65 MHz (up to 20 cores)
- Scaling for moderate Nr. of cores keeps a linear trend
- The modified discretization asks for \approx 40% more computational time
- The level set module only adds \approx 18% of extra computational cost

Summary and Conclusions



- A 2nd order multiphase flow solver is designed by means of coupling LBM and Level set
- Sharp interfaces, low spurious velocities and accurate pressure recovery as compared to monolithic Shan-Chen model
- Large density and viscosity ratios attained using the Averaged-Directional force discretization and MRT collision
- High degree of stability and isotropy via the Averaged-Directional approach
- Maintains the nice properties of LBM; highly scalable for HPC purposes
- Extensive benchmarking; accuracy comparable to that from FEM-based FeatFLOW solutions (www.featflow.de/benchmarks)



Thanks for your attention!





- ▶ Use more robust reinitialization tools for updating the level set
- ▶ Use higher order approximations for normals and curvature
- > Add local multi-block mesh refinements around the interface
- Implementation on graphics processing units (GPU)
- Extend the model towards complex and computationally demanding problems e. g. visco-elastic fluids

The Lattice Boltzmann Method technische universität

The continuous Boltzmann equation discretized in phase space

$$\frac{\partial f_k}{\partial t} + e_k \cdot \nabla f_k = \Omega_c - \frac{F}{\rho} \cdot \nabla_e f$$



Hydrodynamic moments

$$\rho = \sum_{k} f_{k} , \quad \rho u_{i} = \sum_{k} e_{i,k} f_{k}$$

Surface tension boundary condition adds to the N.E. equation via a smeared out delta funcion across the interface Γ

$$\rho(\phi)\partial_t \mathbf{u} + \rho(\phi)\mathbf{u} \cdot \nabla \mathbf{u} + \nabla P - \nabla \cdot \left(\mu(\phi)(\nabla \mathbf{u} + \nabla \mathbf{u}^T)\right) = -\sigma\kappa(\phi)\delta_{\varepsilon}(\phi)\mathbf{n}(\phi)$$

Interface is captured by solving for the implicit level set function

$$\partial_t \phi + \mathbf{u} \cdot \nabla \phi = 0$$
 , $\phi(\mathbf{x}) = 0$ at $X = \Gamma$

 $\boldsymbol{\phi}$ is initialized to and maintained as a "signed distance function"

Normal $\mathbf{n}(\phi)$ and curvature $\kappa(\phi)$ obtained via direct differentiation of ϕ

$$\mathbf{n} = \frac{\nabla \phi}{|\nabla \phi|} \qquad , \qquad \kappa = \nabla \cdot \mathbf{n}$$









► Multiple Relaxation Time LBM

• transform the distribution functions into the moment space

$$\hat{f} = \mathbb{T}f = (\rho, e, e^2, \rho u_x, q_x, \rho u_y, q_y, \sigma_{xx}, \sigma_{yy})^T$$

modify the collision operator for the moment space

$$\Omega = \Lambda(f - f^{eq}) \Rightarrow \Omega = \mathbb{T}^{-1} \hat{\Lambda}(\hat{f} - \hat{f}^{eq})$$

moments relax through their individual relaxation times

$$\hat{\Lambda} = \mathsf{diag}\{ \textit{s}_{0}, \textit{s}_{1}, \textit{s}_{2}, \textit{s}_{3}, \textit{s}_{4}, \textit{s}_{5}, \textit{s}_{6}, \textit{s}_{7}, \textit{s}_{8} \}$$

proper choice of relaxation times is crucial

$$\hat{\Lambda} = \mathsf{diag}\{1, s_1, s_2, 1, s_4, 1, s_4, s_7, s_7\}$$

$$s_1 = 0.3$$
 , $s_2 = 1$, $s_4 = 0.7$, $s_7 = 1/ au$



► Static bubble; Case 1

Pressure profile across the interface





▶ Rising bubble; Test Case 1 \Rightarrow LBM-LS Approach 1, grid effect, 0 < T < 3



Numerical Results



► Relaxation time study



Rising Bubble

Static Bubble

 S_1 corresponds to the energy mode of the flow. A good choice is to under-relax for faster relaxation towards equilibrium!